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European Technical Assessment

ETA-22/0789
of 13.03.2023

General part

Technical Assessment Body issuing the European Technical Assessment

Österreichisches Institut für Bautechnik (OIB)
Austrian Institute of Construction Engineering

Trade name of the construction product

ESSVE screws C-FT, CY-FT, C-PT, W-LF, H-PT, C-FH, H-FT and CY-DT

Product family to which the construction product belongs

Screws for use in timber constructions

Manufacturer

ESSVE Produkter AB
Esbogatan 14
SE-164 74 Kista
P.O.Box 7091, SE-164 07 Kista
Sweden

Manufacturing plant

Manufacturing plant 1

This European Technical Assessment contains

56 pages including 10 Annexes, which form an integral part of this assessment.

This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of

European Assessment Document (EAD)
130118-01-0603 "Screws and threaded rods for use in timber constructions".

Remarks

Translations of the European Technical Assessment in other languages shall fully correspond to the original issued document and should be identified as such.

Communication of this European Technical Assessment, including transmission by electronic means, shall be in full. However, partial reproduction may be made with the written consent of Österreichisches Institut für Bautechnik. Any partial reproduction has to be identified as such.

Specific parts

1 Technical description of the product

This European Technical Assessment (ETA) applies to the screws for use in timber constructions “ESSVE screws C-FT, CY-FT, C-PT, W-LF, H-PT, C-FH, H-FT and CY-DT” hereinafter referred to as ESSVE screws. ESSVE screws are self-tapping screws divided into a drill tip, optionally a compressor and/or cutting groove, thread, optionally a friction part, shank, and head of the screw. The screws are made from special carbon steel and hardened. They are anti-friction coated and are electrogalvanized and passivated (yellow or blue), provided with a zinc-nickel coating or hot-dip galvanized. The washers are made from carbon steel. Possible outer thread diameters as well as overall lengths for the ESSVE screws are given in Table 1.

A bending angle of 45° is reached for all screws.

The screws and washers correspond to the specifications given from Annex 1 to Annex 6. The material characteristics, dimensions and tolerances of the product not indicated in these Annexes, are given in the technical file¹ of the European Technical Assessment.

Table 1: Possible outer thread diameter and overall length of screws

Type of ESSVE screws	Outer thread diameter		Overall length	
	min.	max.	min.	max.
	mm	mm	mm	mm
C-FT-8xL C-FT-10xL C-FT-12xL	8	12	20	1 000
CY-FT-8xL CY-FT-10xL CY-FT-12xL	8	12	20	1 000
C-PT-6xL C-PT-8xL C-PT-10xL C-PT-12xL	6	12	20	500
W-LF-6xL W-LF-8xL W-LF-10xL	6	10	20	500
H-PT-8xL H-PT-10xL H-PT-12xL	8	12	20	500
C-FH-6xL C-FH-8xL C-FH-10xL	6	10	20	500

¹ The technical file of the European Technical Assessment is deposited at Österreichisches Institut für Bautechnik.

Type of ESSVE screws	Outer thread diameter		Overall length	
	min.	max.	min.	max.
	mm	mm	mm	mm
H-FT-12xL	12	12	20	1 000
CY-DT	8	8	120	600

2 Specification of the intended use(s) in accordance with the applicable European Assessment Document

2.1 Intended use

The screws are used for connections in load bearing timber structures between wood-based members or between those members and steel members:

- Solid timber of softwood of strength class C14 or better and solid timber of hardwood of strength class D18 or better according to EN 338² and EN 14081-1,
- Glued laminated timber and glued solid timber of softwood of strength class GL20 or better according to EN 14080 or glued laminated timber of hardwood according to European Technical Assessments (ETA) or national provisions that apply on the installation site,
- Laminated veneer lumber LVL according to EN 14374,
- Cross laminated timber according to European Technical Assessments or national provisions that apply on the installation site.
- Cement-bonded particle boards according EN 634-1 and EN 13986 or ETA or national provisions that apply on the installation site.

The screws may be used for connecting the following wood-based panels to the timber members mentioned above:

- Laminated veneer lumber LVL according to EN 14374 or ETA,
- Solid wood panels according to EN 13353 and EN 13986 or ETA,
- Plywood according to EN 636 and EN 13986 or ETA,
- Oriented strand boards, OSB, according to EN 300 and EN 13986 or ETA,
- Particleboards according to EN 312 and EN 13986 or ETA,
- Fibreboards according to EN 622-2, EN 622-3 and EN 13986 or ETA,
- Cement-bonded particle boards according EN 634-1 and EN 13986 or ETA or national provisions that apply on the installation site,
- Engineered wood products according to ETA, provided that the ETA for the product provides provisions for the use of self-tapping screws and these provisions are applied.

Compression and tension reinforcement perpendicular to the grain with fully threaded screws as well as shear reinforcement with fully threaded screws with a diameter $d \geq 8$ mm is allowed.

In addition, screws with $6 \text{ mm} \leq d \leq 12 \text{ mm}$ may be used for fixing of thermal insulation on rafters and walls.

For engineered wood products according to a European Technical Assessment (ETA) including provisions for the use of self-tapping screws, the provisions of the ETA of the engineered wood product apply.

² Reference documents are listed in Annex 10.

The product shall be subjected to static and quasi static actions only.

The product is intended to be used in service classes 1, 2 and 3 according to EN 1995-1-1. The scope of the screws regarding resistance to corrosion shall be defined according to national provisions that apply at the installation site considering environmental conditions.

Hot-dip galvanised screws with a minimum thickness of the zinc coating of 55 µm may be used in conditions defined by service class 3.

2.2 General assumptions

The screws for use in timber constructions are manufactured in accordance with the provisions of the European Technical Assessment using the manufacturing process as identified in the inspection of the manufacturing plant by Österreichisches Institut für Bautechnik and laid down in the technical file.

The manufacturer shall ensure that the requirements in accordance with the Clauses 1, 2 and 3 as well as with the Annexes of the European Technical Assessment are made known to those who are concerned with design and execution of the works.

Design

The European Technical Assessment only applies to the manufacture and use of the screws for use in timber constructions. Verification of stability of the works including application of loads on the products is not subject to the European Technical Assessment.

The following conditions shall be observed:

- Design of ESSVE screws is carried under the responsibility of an engineer experienced in such products.
- Design of the works shall account for the protection of ESSVE screws to maintain service classes 1, 2 and 3 according to EN 1995-1-1 or national provisions that apply on the installation site.
- ESSVE screws are installed correctly.

Design of the screws for use in timber constructions may be according to EN 1995-1-1, taking into account of Annex 6 to Annex 9 of the European Technical Assessment. Hereby, the outer thread diameter d is used as nominal diameter d or rather effective diameter d_{ef} and l_{ef} is the threaded part in the timber member including point.

Standards and regulations in force at the place of use shall be considered.

Packaging, transport, storage, maintenance, replacement and repair

Concerning product packaging, transport, storage, maintenance, replacement and repair it is the responsibility of the manufacturer to undertake the appropriate measures and to advise his clients on the transport, storage, maintenance, replacement and repair of the product as he considers necessary.

Installation

It is assumed that the product will be installed according to the manufacturer's instructions or (in absence of such instructions) according to the usual practice of the building professionals.

The screws are either driven into the wood-based member of softwood without pre-drilling or in predrilled holes with a diameter not exceeding the inner thread diameter or rather into the wood-based member of hardwood in predrilled holes with a diameter minimally exceeding the inner thread diameter.

The screw holes in steel members shall be pre-drilled with an adequate diameter greater than the outer thread diameter.

The minimum penetration length of screws in the load-bearing wood-based members shall be 4 d .

Screws made of carbon steel with an outer thread diameter $6 \text{ mm} \leq d \leq 12 \text{ mm}$ may be driven into laminated veneer lumber LVL of beech or related products of hardwood with predrilling.

At least four screws shall be used in a connection with screws ($6 \text{ mm} \leq d \leq 12 \text{ mm}$) inserted in the timber member with an angle between screw axis and grain direction of less than 15° . The penetration length of the threaded part of the partly or fully threaded screw shall be at least $20 d$.

The use of only one screw in load-bearing connections is possible for screws ($6 \text{ mm} \leq d \leq 12 \text{ mm}$) loaded in axial direction and angles between grain direction and screw axis $\alpha \geq 15^\circ$ provided that a minimum penetration length of the threaded part of the screw of $20 d$ can be ensured. Hereby, the load-bearing capacity of the screw must be reduced by 50%. This reduction is not necessary for screws used as reinforcement perpendicular to the grain of wood-based members.

To ensure a proper installation for screws with lengths of more than 800 mm a guiding hole of $5 d$ is recommended.

For mounting of steel plates and wood-based panels the screw head must be placed on top of these members.

The structural members which are connected with ESSVE screws shall

- be in accordance with Clause 2.1;
- ensure minimum spacing and edge distances in accordance with EN 1995-1-1 and Annex 6.

2.3 Assumed working life

The provisions made in the European Technical Assessment (ETA) are based on an assumed intended working life of ESSVE screws of 50 years, when installed in the works, provided that the screws are subject to appropriate installation, use and maintenance (see Clause 2.2). These provisions are based upon the current state of the art and the available knowledge and experience³.

The indications given as to the working life of the construction product cannot be interpreted as a guarantee neither given by the product manufacturer or his representative nor by EOTA nor by the Technical Assessment Body, but are regarded only as a means for choosing the appropriate products in relation to the expected economically reasonable working life of the works.

³ The real working life of a product incorporated in a specific works depends on the environmental conditions to which that works is subject, as well as on the particular conditions of the design, execution, use and maintenance of that works. Therefore, it cannot be excluded that in certain cases the real working life of the product can also be shorter than the assumed working life.

3 Performance of the product and reference to the methods used for its assessment

3.1 Essential characteristics of the product

Table 2: Essential characteristics of the product and product performance

No	Essential characteristic	Product performance
Basic requirement for construction works 1: Mechanical resistance and stability ¹⁾		
1	Dimensions	Annex 1 to Annex 5
2	Characteristic yield moment	Annex 6
3	Bending angle	Clause 1
4	Characteristic withdrawal parameter	Annex 6
5	Characteristic head pull-trough parameter	Annex 6
6	Characteristic tensile strength	Annex 6
7	Characteristic yield strength	Annex 6
8	Characteristic torsional strength	Annex 6
9	Insertion moment	Annex 6
10	Spacing, end and edge distances of the screws and minimum thickness of the wood based material	Annex 6
11	Slip modulus for mainly axially loaded screws	Annex 6
12	Durability against corrosion	3.1.1
Basic requirement for construction works 2: Safety in case of fire		
13	Reaction to fire	3.1.2
Basic requirement for construction works 4: Safety and accessibility in use		
14	Same as BWR 1	
¹⁾ These characteristics also relate to basic requirement 4 for construction works.		

3.1.1 Durability against corrosion

The product is intended to be used in service classes 1, 2 and 3 according to EN 1995-1-1.

The screws and washers made from carbon steel are electrogalvanized and yellow or blue passivated, coated with a zinc-nickel coating or hot-dip galvanized. The minimum thickness of the zinc coating of the screws is 5 µm and the minimum thickness of the zinc-nickel coating is 4 µm. The minimum thickness of the zinc coating of hot-dip galvanized screws is 55 µm.

Durability of ESSVE screws is in accordance with EN 1995-1-1 or national provisions that apply on the installation site.

3.1.2 Reaction to fire

ESSVE screws are made from steel classified as Euroclass A1 in accordance with Commission Decision 96/603/EC, as amended by Commission Decision 2000/605/EC.

3.2 Assessment methods

3.2.1 General

The assessment of the essential characteristics in Clause 3.1 of the screws for use in timber constructions for the intended use, and in relation to the requirements for mechanical resistance and stability, for safety in case of fire and for safety and accessibility in use in the sense of the basic requirements for construction works № 1, 2 and 4 of Regulation (EU) № 305/2011 has been made in accordance with the European Assessment Document EAD 130118-01-0603, "Screws and threaded rods for use in timber constructions".

3.2.2 Identification

The European Technical Assessment for the screws for use in timber constructions is issued on the basis of agreed data that identify the assessed product. Changes to materials, to composition, to characteristics of the product, or to the production process could result in these deposited data being incorrect. Österreichisches Institut für Bautechnik should be notified before the changes are implemented, as an amendment of the European Technical Assessment is possibly necessary.

4 Assessment and verification of constancy of performance (thereinafter AVCP) system applied, with reference to its legal base

4.1 System of assessment and verification of constancy of performance

According to Commission Decision 97/176/EC the system of assessment and verification of constancy of performance to be applied to "ESSVE screws C-FT, CY-FT, C-PT, W-LF, H-PT, C-FH, H-FT and CY-DT" is System 3. System 3 is detailed in Commission Delegated Regulation (EU) № 568/2014 of 18 February 2014, Annex, 1.4., and provides for the following items

- (a) The manufacturer shall carry out factory production control.
- (b) The notified laboratory shall assess the performance on the basis of testing (based on sampling carried out by the manufacturer), calculation, tabulated values or descriptive documentation of the construction product.

4.2 AVCP for construction products for which a European Technical Assessment has been issued

Notified bodies undertaking tasks under System 3 shall consider the European Technical Assessment issued for the construction product in question as the assessment of the performance of that product. Notified bodies shall therefore not undertake the tasks referred to in point 4.1 (b).

5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable European Assessment Document

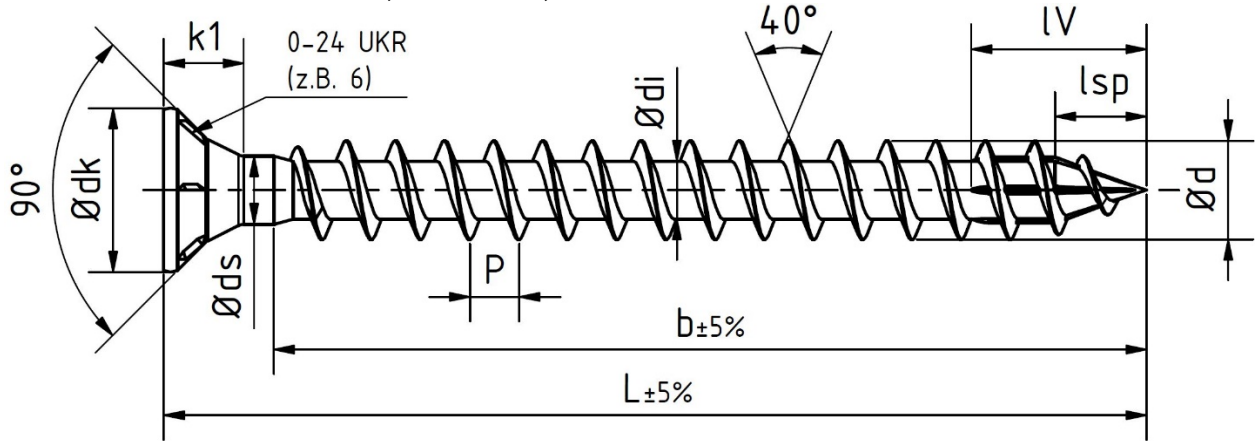
5.1 Tasks for the manufacturer

5.1.1 Factory production control

In the manufacturing plant the manufacturer shall establish and continuously maintain a factory production control. All procedures and specifications adopted by the manufacturer shall be documented in a systematic manner. The factory production control shall ensure the constancy of performances of ESSVE screws with regard to the essential characteristics.

The manufacturer shall only use raw materials supplied with the relevant inspection documents as laid down in the control plan. The incoming raw materials shall be subject to controls by the manufacturer before acceptance. Check of incoming materials shall include control of inspection documents presented by the manufacturer of the raw materials.

Countersunk head “C-FT-8xL, C-FT-10xL, C-FT-12xL”

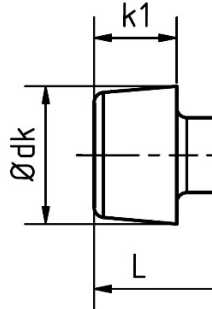


UKR ... cutter ribs

Dim	Ødk	k1	Øds	Ød	Ødi	P	lsp	Ødn	ØdV	a
8,0	15,0 ±1.20	7,0 ±0.70	5,9 ±0.29	8,0 ±0.40	5,10 ±0.26	3,8 ±0.38	8,2 ±2.1	7,2 ±0.72	6,0 ±0.60	11,0 ±2.5
10,0	18,5 ±1.50	9,0 ±0.90	7,1 ±0.35	10,0 ±0.60	6,30 ±0.32	4,6 ±0.46	10,1 ±2.3	8,6 ±0.86	7,1 ±0.72	13,0 ±3.0
12,0	21,0 ±2.00	10,0 ±1.00	8,2 ±0.41	12,0 ±0.70	7,00 ±0.35	6,0 ±0.60	11,2 ±2.6	9,6 ±0.96	7,9 ±0.80	15,0 ±3.0

IV = 2P to 4P

Cylinder head “CY-FT-8xL, CY-FT-10xL, CY-FT-12xL”



Dim	Ødk	k1
8,0	10,2 ±0.51	7,5 ±1.0
10,0	13,4 ±0.67	8,0 ±1.0
12,0	14,2 ±0.71	10,0 ±1.5

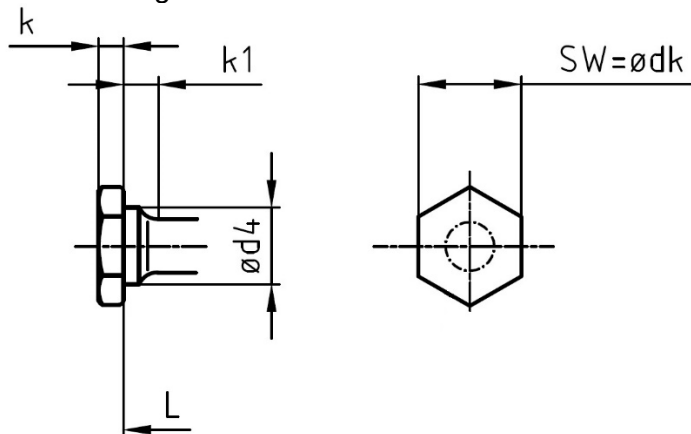
ESSVE screws

C-FT-8-12xL
CY-FT-8-12xL
H-FT-12xL

Annex 1

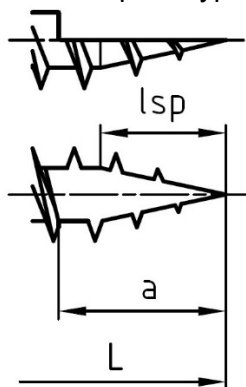
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Kombi hexagonal head "H-FT-12xL"

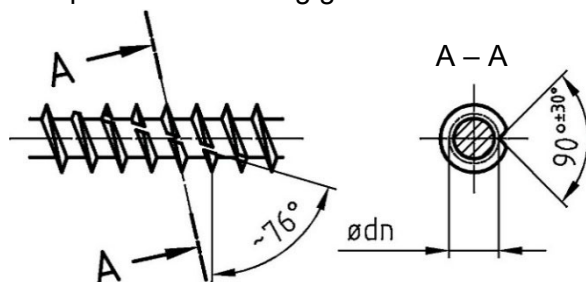


Dim	SW=∅dk	k	k1	∅d4
12,0	17,0 -0,85	5,5 ±1.3	10,0 ±2.0	12,0 ±1.20

Alternative point type: Half cut (HSP)



Detail: optional with cutting groove



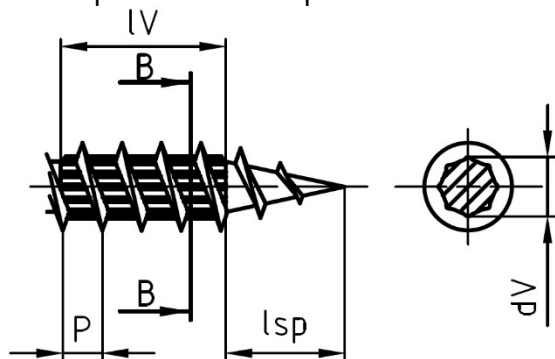
ESSVE screws

C-FT-8-12xL
CY-FT-8-12xL
H-FT-12xL

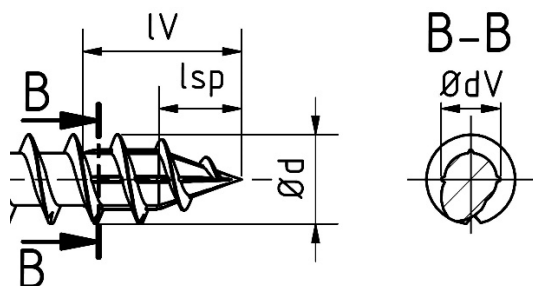
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Detail: optional with compressor or alternative compressor



Number of flanks: 4 – 8
 $IV = 2P \text{ to } 4P$



Screw length L and thread length of the screw b					
Dim. 8.0		Dim. 10.0		Dim. 12.0	
L	b	L	b	L	b
50-400	L-10	50-300	L-12	60-300	L-20
>400	L-23	>300	L-24	>300	L-25

threaded part of the screw $b = b_{\min}$:
 $b_{\max} = L - k_1$

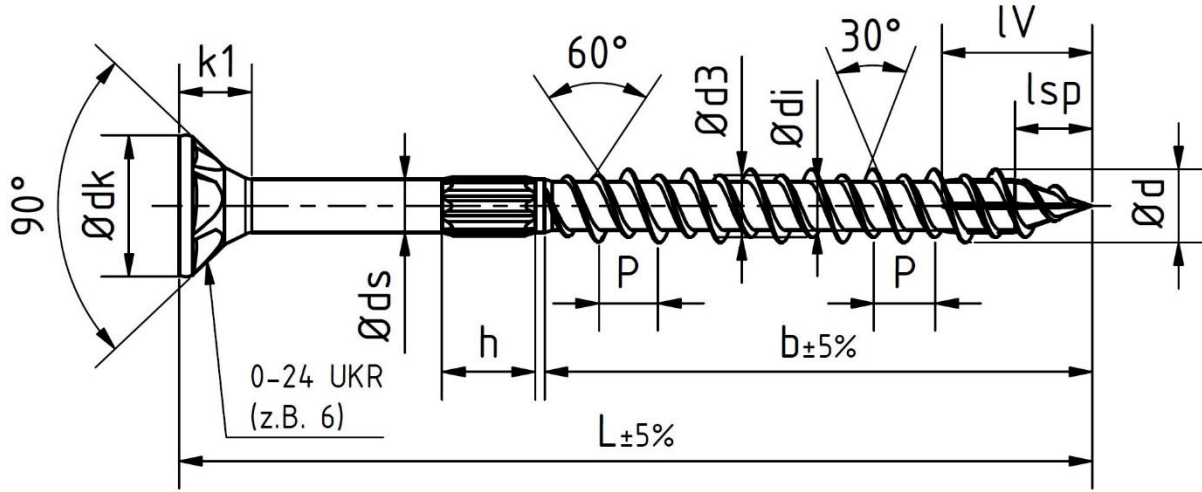
ESSVE screws

C-FT-8-12xL
 CY-FT-8-12xL
 H-FT-12xL

Annex 1

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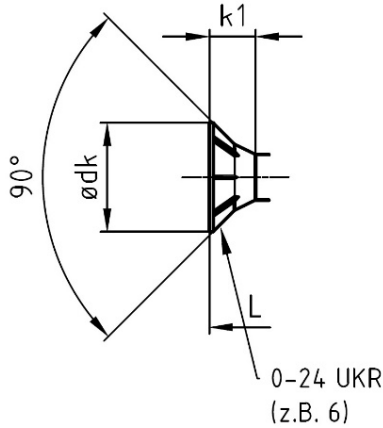
Countersunk head „C-PT-6xL, C-PT-8xL, C-PT-10xL“



Dim	Ødk	k1	Øds	Ød	Ødi	Ød3	P	lsp	Ødn	ØdR	h	ØdV
6,0	12,0 ±0.90	5,5 ±0.55	4,3 ±0.21	6,0 ±0.30	4,00 ±0.20	5,0 ±0.25	5,0 ±0.50	7,3 ±1.9	5,4 ±0.54	4,7 ±0.5	10,2 ±1.0	4,4 ±0.44
8,0	15,0 ±1.20	7,0 ±0.70	5,9 ±0.29	8,0 ±0.40	5,35 ±0.27	6,8 ±0.34	6,7 ±0.67	8,2 ±2.1	7,2 ±0.72	6,2 ±0.6	10,2 ±1.0	6,0 ±0.60
10,0	18,5 ±1.50	9,0 ±0.90	7,1 ±0.35	10,0 ±0.60	6,80 ±0.34	7,9 ±0.40	7,9 ±0.79	10,1 ±2.3	8,6 ±0.86	7,7 ±0.8	10,2 ±1.0	7,1 ±0.72

IV = 2P to 4P

Alternative countersunk head with UKR (cutter ribs)



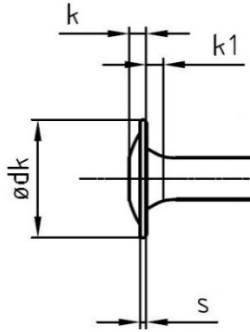
ESSVE screws

- C-PT-6-10xL
- W-LF-6-10xL
- H-PT-8-10xL
- C-FH-6-10xL

Annex 2

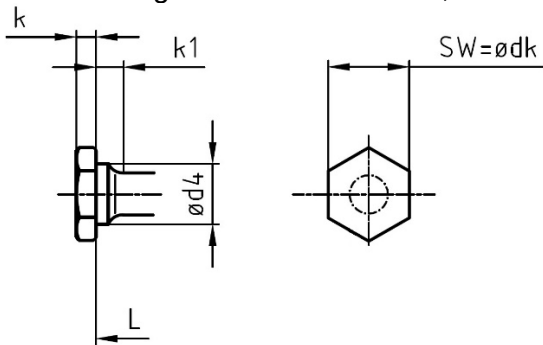
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Washer head “W-LF-6xL, W-LF-8xL, W-LF-10xL”



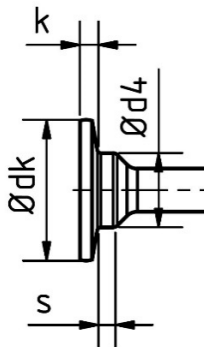
Dim	Ødk	k	k1	s
6,0	14,0 ±0.80	3,0 ±1.0	1,4 ±0.8	1,5 ±0.8
8,0	20,0 ±1.50	3,5 ±1.0	1,9 ±1.0	2,0 ±0.9
10,0	25,0 ±2.00	4,5 ±1.2	2,6 ±1.5	2,0 ±0.9

Kombi hexagonal head “H-PT-8xL, H-PT-10xL”



Dim	SW=Ødk	k	k1	Ød4
8,0	12,0 -0,60	4,5 ±1.3	6,3 ±1.0	8,0 ±0.80
10,0	15,0 -0,75	5,0 ±1.3	8,0 ±1.5	10,0 ±1.00

Flat head “C-FH-6xL, C-FH-8xL, C-FH-10xL”



Dim	Ødk	k	s	Ød4
6,0	13,0 ±0.65	1,8 ±1.0	1,8 ±1.0	8,0 ±0.4
8,0	19,0 ±1.50	2,4 ±1.0	2,4 ±1.0	10,0 ±0.5
10,0	24,0 ±2.50	3,0 ±1.0	3,0 ±1.0	13,0 ±0.65

ESSVE screws

- C-PT-6-10xL
- W-LF-6-10xL
- H-PT-8-10xL
- C-FH-6-10xL

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Screw length L and thread length of the screw b					
Dim. 6.0		Dim. 8.0		Dim. 10.0	
L	b	L	b	L	b
50	30	50	30	60-70	40
60-70	40	60-70	40	80	50
80-90	50	80-90	50	100	60
100-110	60	100	60	120-160	80
120-300	70	120-160	80	180-500	100
		180-500	100		

threaded part of the screw $b = b_{\min}$:

b_{\max} (fully threaded screw) = $L - k_1$

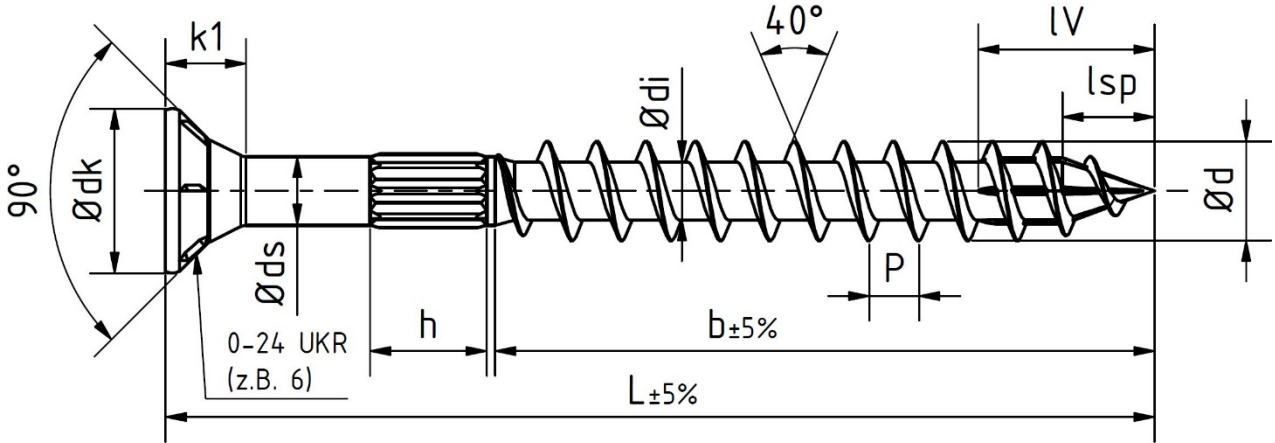
ESSVE screws

C-PT-6-10xL
W-LF-6-10xL
H-PT-8-10xL
C-FH-6-10xL

Annex 2

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Countersunk head "C-PT-12xL"

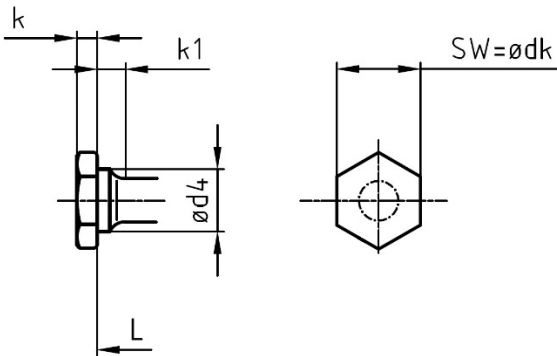


UKR ... cutter ribs

Dim	Ødk	k1	Øds	Ød	Ødi	P	lsp	Ødn	ØdR	h	ØdV
12,0	21,0 ±2.00	10,0 ±1.00	8,2 ±0.41	12,0 ±0.70	7,00 ±0.35	6,0 ±0.60	11,2 ±2.6	8,9 ±0.89	9,0 ±0.9	14,2 ±1.0	7,9 ±0.80

IV = 2P to 4P

Kombi hexagonal head "H-PT-12xL"



Dim	SW=Ødk	k	k1	Ød4
12,0	17,0 -0,85	5,5 ±1.3	10,0 ±2.0	12,0 ±1.20

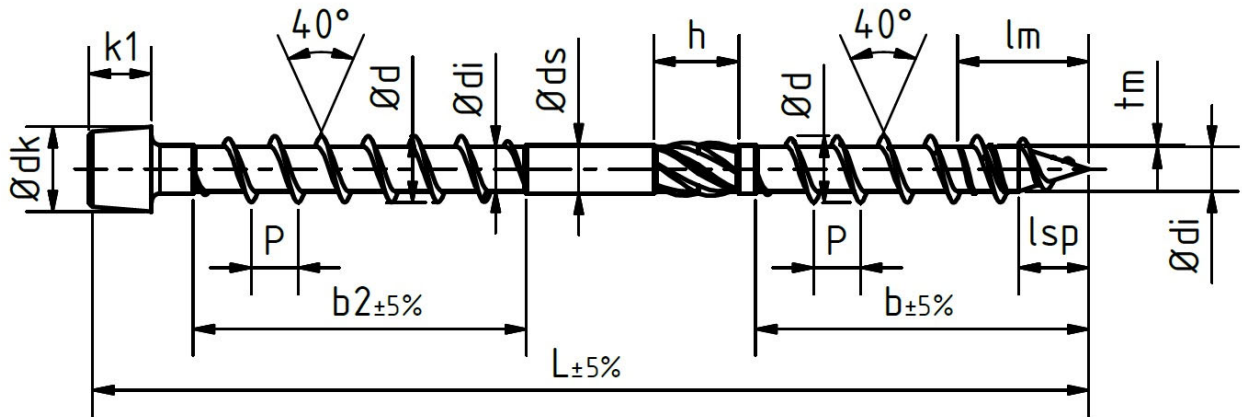
ESSVE screws

C-PT-12xL
H-PT-12xL

Annex 3

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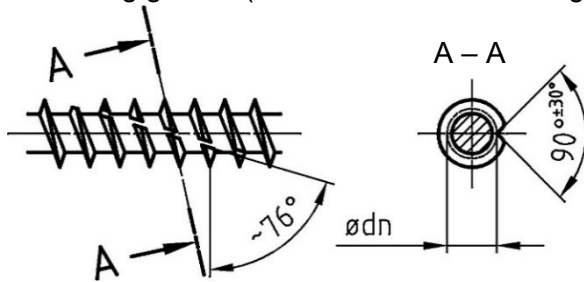
Cylinder head "CY-DT"



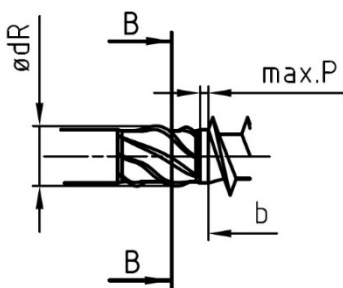
Dim	Ødk	k1	Øds	Ød	Ødi	P	lsp	Ødn	ØdR	h	tm
8,0	10,2 ±0.51	7,5 ±1.0	5,9 ±0.29	8,0 ±0.40	5,30 ±0.26	5,6 ±0.56	8,2 ±2.1	7,2 ±0.72	6,8 ±0.6	10,2 ±1.0	0,60 ±0.12

$l_m = l_{sp} + 1.0 P$

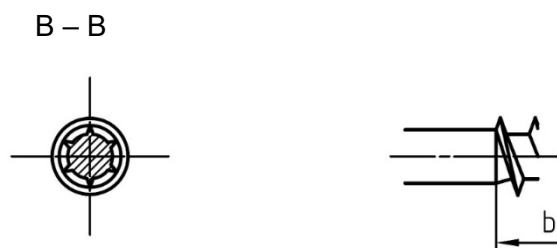
Detail: cutting groove (alternative without cutting groove)



Detail: friction part



alternative without friction part



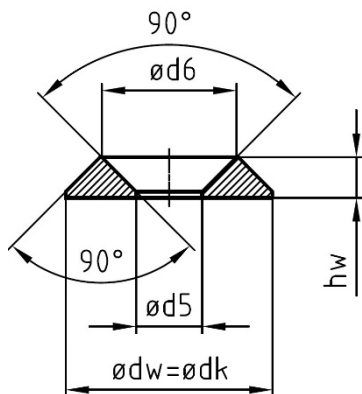
ESSVE screws

CY-DT

Annex 4

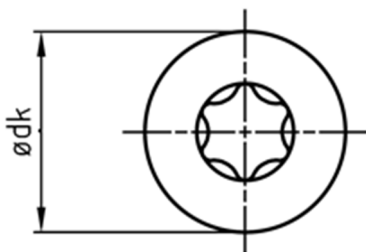
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Washer (for screws with 90° head, only)



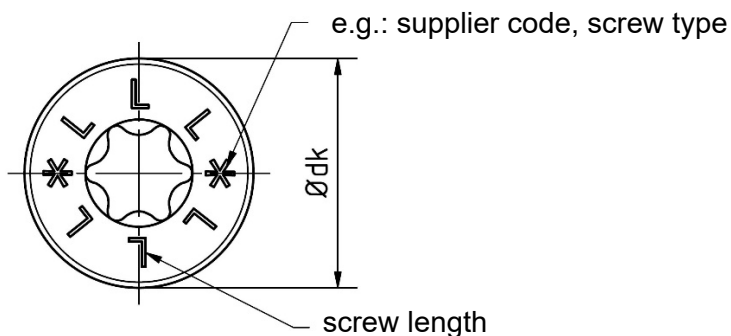
Dim	Ødw=Ødk	Ød5	Ød6	hw
6,0	22,0 ±2.0	8,5 ±2.0	13,5 ±1.5	4,5 ±1.0
8,0	28,0 ±2.0	10,0 ±2.0	17,5 ±2.0	5,5 ±1.0
10,0	35,0 ±3.0	12,0 ±2.0	22,5 ±2.2	6,5 ±1.5
12,0	42,0 ±3.0	14,0 ±2.0	25,0 ±2.5	7,5 ±1.5

T-Drive



Dim	T
4,0	T10 / T15 / T20
4,5	T15 / T20 / T25
5,0	T20 / T25 / T30
6,0	T20 / T25 / T30
7,0	T25 / T30
8,0	T30 / T40
10,0	T40 / T50
12,0	T40 / T50 / T55

head labelling optional



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Drive types and head labelling

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A.6 Load bearing capacity of ESSVE screws

The characteristic load bearing capacities in Tables A6.1 to A6.3 are given for timber of strength class C24 according to EN 338 ($\rho_{k,ref} = 350 \text{ kg/m}^3$) unless specified otherwise in the following.

If relevant, the design block shear failure resistance of a timber member has to be proven.

Table A6.1: Characteristic load bearing capacities of ESSVE screws C-FT, CY-FT and H-FT; screw diameter 8 to 12 mm

Product characteristic			Screw diameter ¹⁾		
			8	10	12
Max. length	l_{max}	mm	1000	1000	1000
Characteristic tensile strength	$f_{tens,k}$	kN	24.1	40.0	46.7 45.0 ²⁾
Characteristic yield moment	$M_{y,k}$	Nm	20.3	36.7	48.5
Characteristic withdrawal parameter angle screw-axis to grain: 90° ($\rho_{k,ref} = 350 \text{ kg/m}^3$)	$f_{ax,k,90^\circ}$	N/mm ²	13.1	12.5	11.2
Characteristic yield strength	$f_{y,k}$	N/mm ²	950		
Characteristic torsional strength	$f_{tor,k}$	Nm	25.8	55.0	73.0
Ratio characteristic torsional strength to mean insertion moment $\rho_{k,ref} = 450 \text{ kg/m}^3$	$f_{tor,k} / R_{tor,m}$	-	≥ 1.5	≥ 1.5	≥ 1.5
Slip modulus	K_{ser}	N/mm	see A.6.1.7		

¹⁾ For intermediate screw diameters the conservative value of the next screw diameter may be used.

²⁾ H-FT-12xL

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Table A6.2: Characteristic load bearing capacities of ESSVE screws C-PT, W-LF, H-PT and C-FH; screw diameter 6 to 12 mm

Product characteristic			Screw diameter ¹⁾			
			6	8	10	12
Max. length	l_{max}	mm	300	500	500	500
Characteristic tensile strength	$f_{tens,k}$	kN	13.1	23.3	35.0	42.0
Characteristic yield moment	$M_{y,k}$	Nm	10.7	22.6	33.6	46.9
Characteristic withdrawal parameter angle screw-axis to grain: 90° ($\rho_{k,ref} = 350 \text{ kg/m}^3$)	$f_{ax,k,90^\circ}$	N/mm ²	13.0	10.9	11.0	11.2
Characteristic yield strength	$f_{y,k}$	N/mm ²	900			
Characteristic torsional strength	$f_{tor,k}$	Nm	10.9	28.0	52.5	59.6
Ratio characteristic torsional strength to mean insertion moment $\rho_{k,ref} = 450 \text{ kg/m}^3$	$f_{tor,k} / R_{tor,m}$	-	≥ 1.5			

¹⁾ For intermediate screw diameters the conservative value of the next screw diameter may be used.

Table A6.3: Characteristic load bearing capacities of ESSVE screws CY-DT; screw diameter 8 mm

Product characteristic			Screw diameter
			8
Max. length	l_{max}	mm	600 ¹⁾
Characteristic tensile strength	$f_{tens,k}$	kN	22.0
Characteristic yield moment	$M_{y,k}$	Nm	21.0
Characteristic withdrawal parameter angle screw-axis to grain: 90° ($\rho_{k,ref} = 350 \text{ kg/m}^3$)	$f_{ax,k,90^\circ}$	N/mm ²	13.1
Characteristic yield strength	$f_{y,k}$	N/mm ²	900
Characteristic torsional strength	$f_{tor,k}$	Nm	24.8
Ratio characteristic torsional strength to mean insertion moment $\rho_{k,ref} = 450 \text{ kg/m}^3$	$f_{tor,k} / R_{tor,m}$	-	≥ 1.5

¹⁾ $l > 500 \text{ mm}$ for screws with friction part, only.

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Table A6.4: Minimum spacing, end and edge distances of only axially loaded ESSVE screws (except CLT)

Designation		Variant 1	Variant 2
Boundary condition	$a_1 \cdot a_2$	$\geq 25 d^2$	$\geq 21 d^2$
Spacing in a plane parallel to the grain	a_1	$5 d$	$7 d$
Spacing perpendicular to a plane parallel to the grain	a_2	$2.5 d$	$3 d$
Spacing between the crossing screws for a crossed screw couple perpendicular to a plane parallel to the grain	a_{cross}	$1.5 d$	
End distance of the centre of gravity of the threaded part in the timber member	$a_{1,c}$	$5 d$	
Edge distance of the centre of gravity of the threaded part in the timber member	$a_{2,c}$	$4 d$	

Provided that a minimum thickness of the cross laminated timber of $10 d$ as well as a minimum penetration length of the screws of $4 d$ in the wide face or $10 d$ in the narrow face are met, the minimum spacings, end and edge distances given in Table A6.5 apply.

Table A6.5: Minimum spacings, end and edge distances of ESSVE screws in cross laminated timber (axially and/or laterally loaded)

	a_1	$a_{3,t}$	$a_{3,c}$	a_2	$a_{4,t}$	$a_{4,c}$
Wide face (see Figure A6.1)	$4 d$	$6 d$	$6 d$	$2.5 d$	$6 d$	$2.5 d$
Narrow face (see Figure A6.1)	$10 d$	$12 d$	$7 d$	$3 d$	$5 d$	$3 d$

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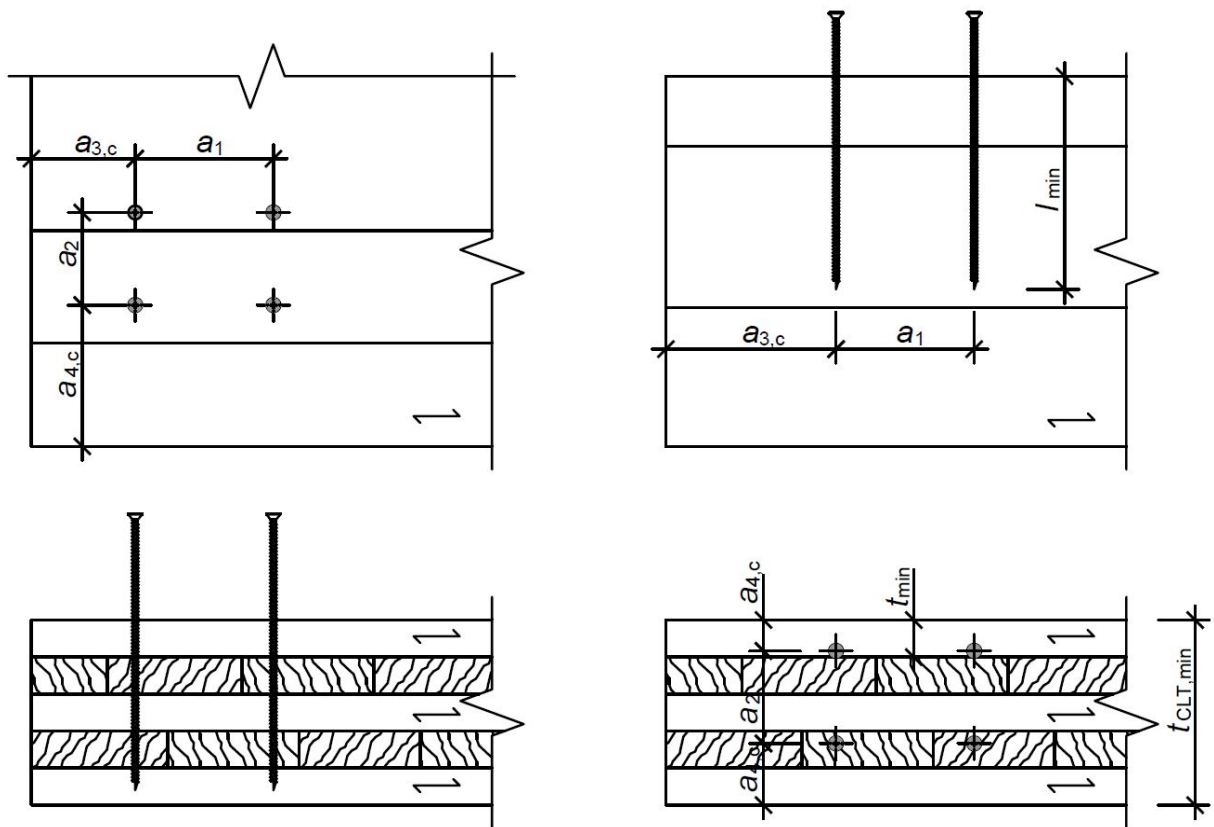


Figure A6.1: Definition of minimum spacings, end and edge distances in the wide face (left) and narrow face (right) of cross laminated timber

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A.6.1.3 Characteristic withdrawal parameter

The characteristic withdrawal parameter for ESSVE screws for angles $0^\circ \leq \alpha \leq 90^\circ$ between screw-axis and direction of wood-fibre may be calculated as

$$f_{ax,calc,k} = f_{ax,k,90^\circ} \cdot k_{ax} \cdot k_{sys} \cdot \left(\frac{\rho_k}{\rho_{k,ref}} \right)^{k_p}$$

$$k_{ax} = \begin{cases} 1.0 & \text{for } 30^\circ \leq \alpha \leq 90^\circ \\ 0.3 \cdot k_{gap} + \frac{\alpha}{30^\circ} (1 - 0.3 \cdot k_{gap}) & \text{for } 0^\circ \leq \alpha \leq 30^\circ \end{cases}$$

$$k_{gap} = \begin{cases} 0.9 & \text{for narrow face in CLT} \\ 1.0 & \text{other} \end{cases}$$

$$k_{sys} = \begin{cases} 1.0 & \text{for solid timber} \\ \text{see Table A6.6} & \text{for layered timber} \end{cases}$$

$$k_p = \begin{cases} 1.10 & \text{for softwood and } 15^\circ \leq \alpha \leq 90^\circ \\ 1.25 - 0.05 d & \text{for softwood and } 0^\circ \leq \alpha \leq 15^\circ \\ 1.40 & \text{for ring porous hardwood and } 0^\circ \leq \alpha \leq 90^\circ \\ 1.70 & \text{for diffuse porous hardwood and } 0^\circ \leq \alpha \leq 90^\circ \end{cases}$$

Examples for ring porous hardwoods: chestnut, ash, oak
 Examples for diffuse porous hardwoods: poplar, birch, beech

$f_{ax,k,90^\circ}$ characteristic withdrawal parameter according to Tables 6.1 to 6.3 in N/mm²

$\rho_{k,ref}$ reference characteristic density of timber raw material in kg/m³ in which the screw is driven (350 kg/m³ (C24) for Tables A6.1 to A6.3)

ρ_k characteristic density of timber in kg/m³

α angle between screw axis and grain direction

k_{sys} system factor according to Table A6.6

n number of screwed layers

Table A6.6: System factor k_{sys} depending on the number of layers n for screw insertion in GLT or CLT

n	1	2	3	4	5	≥ 6
k_{sys}	1.00	1.06	1.10	1.12	1.13	1.15

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A.6.1.5 Characteristic head pull-through capacity for wood based panels

The characteristic value of the head pull-through parameter for a characteristic density of 380 kg/m³ of the timber and for the following wood based panels

- Plywood according to EN 636 and EN 13986,
- Oriented strand boards, OSB, according to EN 300 and EN 13986,
- Solid wood panels according to EN 13353 and EN 13986,
- Particleboard according to EN 312 and EN 13986,
- Fibreboards according to EN 622-2, EN 622-3 and EN 13986,
- Cement-bonded particle boards according to EN 634-1 and EN 13986

is given in Table A6.9.

Table A6.9: Characteristic value of the head pull-through parameter in dependence of the thickness of the wood-based panels t_{WBP}

t_{WBP}	≤ 12 mm	12 mm $< t_{WBP} \leq 20$ mm	> 20 mm
$f_{head,k}$	8 N/mm ² *	8 N/mm ²	10 N/mm ²
* limited to 400 N complying with the minimum thicknesses of the wood based panels of 1.2 d, with d as outer thread diameter			

For plywood with a minimum of 7 layers and a minimum thickness of 18 mm, the characteristic value of the head pull-through parameter for a characteristic density of 490 kg/m³ is ($d_k \geq 18.8$ mm)

$f_{head,k} = 16$ N/mm²

In addition the minimum thicknesses of Table A6.10 apply.

Table A6.10 Minimum thicknesses of wood based panels

Wood based panel	Minimum thickness in mm
Plywood	6
Oriented strand board, OSB	8
Solid wood panels	12
Particleboard	8
Fibreboards	6
Cement-bonded particle boards	8

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A.6.1.6 Compressive loading for fully threaded screws

The design load carrying capacity for ESSVE screws with a full thread for an angle $30^\circ \leq \alpha \leq 90^\circ$ between screw-axis and direction of wood-fibre for axial compressive loading is given as

$$F_{ax,Rd} = \min \left(f_{ax,calc,k} \cdot d \cdot l_{ef} \cdot \frac{k_{mod}}{\gamma_M}; \kappa_c \cdot \frac{N_{pl,k}}{\gamma_{M1}} \right)$$

with

$f_{ax,calc,k}$ char. withdrawal capacity of the threaded part of the screw according to Clause A.6.1.3 in N/mm²

d outer thread diameter of the screw in mm

l_{ef} penetration length of the threaded part of the screw in the timber member in mm

k_{mod} modification factor for duration of load and moisture content according to EN 1995-1-1

γ_M partial safety factor for connections according to EN 1995-1-1

γ_{M1} partial safety factor according to EN 1993-1-1

$$\kappa_c = \begin{cases} 1.0 & \text{for } \bar{\lambda}_k \leq 0.2 \\ \frac{1.0}{k + \sqrt{k^2 - \bar{\lambda}_k^2}} & \text{for } \bar{\lambda}_k > 0.2 \end{cases}$$

$$k = 0.5 \left[1 + 0.49 \cdot (\bar{\lambda}_k - 0.2) + \bar{\lambda}_k^2 \right]$$

The related slenderness ratio

$$\bar{\lambda}_k = \sqrt{\frac{N_{pl,k}}{N_{ki,k}}}$$

with

$N_{pl,k}$ characteristic value of the plastic normal force load bearing capacity of the net cross-section, related to the inner thread diameter d_i (or shank diameter d_s if relevant) of the screws in N

$$N_{pl,k} = \frac{\pi \cdot d_i^2}{4} \cdot f_{y,k}$$

$f_{y,k}$ characteristic yield strength of ESSVE screws in N/mm² according to Table A6.1 to A6.3

$N_{ki,k}$ characteristic ideal elastic buckling load in N

$$N_{ki,k} = \sqrt{c_h \cdot E_s \cdot I_s}$$

c_h elastic foundation of the ESSVE screws in the wooden member in N/mm²

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$$c_h = (0.19 + 0.012 \cdot d) \cdot \rho_k \cdot \left(\frac{90 + \alpha}{180}\right)$$

E_s modulus of elasticity of ESSVE screws in N/mm², $E_s = 210\,000$ N/mm²

I_s area moment of inertia of ESSVE screws in mm⁴

ρ_k characteristic density of the wood-based member in kg/m³

$$I_s = \frac{\pi \cdot d_i^4}{64}$$

A.6.1.7 Slip modulus for mainly axially loaded screws

The axial slip modulus $K_{ser,ax}$ of the threaded part per cutting surface for the serviceability limit state shall be taken for screws independent of angle α to the grain as

$$K_{ser,ax} = k_{HA} \cdot d \cdot l_{ef} \text{ in N/mm}$$

with

d outer thread diameter of the screw in mm

l_{ef} penetration length of the threaded part of the screw in the timber member in mm

k_{HA} coefficient depending on the type of wood of the wood-based member according to Table A6.11

Table A6.11: Coefficient k_{HA} depending on the type of wood of the wood-based member

Type of wood	Reference density ρ_m in kg/m ³	Coefficient k_{HA}
softwood	420	25
chestnut	530	48
ash	660	62
poplar	485	34
birch	635	54
beech	740	78
LVL beech*	840	53
* according to EN 14374 or European Technical Assessment		

The coefficients listed in Table A6.11 apply to ESSVE screws installed with or without pre-drilling, provided that the pre-drilling diameter does not exceed 75% of the outer thread diameter.

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A.6.2 Laterally loaded screws (perpendicular to the screw axis)

A.6.2.1 General

For verification of the load bearing capacity of laterally loaded ESSVE screws the failure mechanisms according to EN 1995-1-1 as well as the minimum thicknesses, spacings and distances according to A.6.2.2 must be taken into account.

NOTES:

- 1) Hereby, the outer thread diameter d is used as effective diameter of the screw in accordance with EN 1995-1-1.
- 2) For connections between timber and a steel member where the special head shape of the ESSVE screws enables a precise fit into the drilling of the steel member the equations for thick steel may be used in case of steel thicknesses $t \geq 1.5$ mm. The height of the flange must be greater than the thickness of the steel member.
- 3) In the case of a connection with a group of screws loaded perpendicular to the screw axis the effective number of screws is to be taken as for nails according to EN 1995-1-1 if the connection area of the timber is not reinforced according to Clause A.8.2.3.

A.6.2.2 Spacing, end and edge distances of the screws and minimum thicknesses

For ESSVE screws which are loaded only laterally, the minimum spacing, end and edge distances according to Table A6.12 apply.

Table A6.12: Minimum spacing, end and edge distances of only laterally loaded ESSVE screws

Type	Spacing/distances
Predrilled wooden members or ESSVE screws with HSP in non-predrilled holes of softwood members	Analogous to pre-drilled nails according to EN 1995-1-1
Non-predrilled wooden members with ESSVE screws without HSP	Analogous to non-predrilled nails according to EN 1995-1-1

NOTES:

- 1) For screws with outer thread diameter $d \geq 8$ mm in non-predrilled holes in wood-based members with thickness $t < 5 d$, the minimum distances for loaded and unloaded ends shall be $15 d$.
- 2) Minimum distances from the unloaded edge perpendicular to the grain may be reduced to $3 d$ also for timber thickness $t < 5 d$, if the spacing parallel to the grain and the end distance is at least $25 d$.
- 3) Minimum spacings, end and edge distances of laterally loaded ESSVE screws in wide face and narrow face of cross laminated timber are given in Table A6.5.

The minimum thickness for structural members shall be in accordance with Table A6.13.

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Table A6.13: Minimum thickness for structural members for laterally loaded ESSVE screws $d \leq 12$ mm

Screw diameter		< 8	8	10	12
Minimum thickness t for structural members	mm	24	30	40	80

A.6.2.3 Characteristic embedment strength

EN 1995-1-1 applies for the embedment strength of ESSVE screws in wooden members unless specified otherwise below.

The characteristic embedment strength of ESSVE screws installed in wooden members of solid wood, glued laminated timber, glued solid timber, solid wood panels or laminated veneer lumber (made of softwood) may be determined as follows:

$$f_{h,k} = k_{\alpha} \cdot k_{\beta} \cdot k_{\varepsilon} \cdot f_{h,k,ref} \text{ in N/mm}^2$$

with

$f_{h,k,ref}$ as reference characteristic embedment strength, for non-predrilled members

$$f_{h,k,ref} = 0.082 \cdot \rho_k \cdot d^{-0.3} \text{ in N/mm}^2$$

and for pre-drilled members

$$f_{h,k,ref} = 0.082 \cdot \rho_k \cdot (1 - 0.01 \cdot d) \text{ in N/mm}^2$$

and

$$k_{\alpha} = \frac{1}{2.5 \cdot \cos^2 \alpha + \sin^2 \alpha}$$

α angle between screw axis and grain direction

$$k_{\beta} = \begin{cases} \frac{1.0}{1.5 \cdot \cos^2 \beta + \sin^2 \beta} & \text{screws inserted in LVL made of softwood} \\ 1.0 & \text{others} \end{cases}$$

β angle between screw axis and the wide face of LVL

$$k_{\varepsilon} = k_{90} \cdot \cos^2 \varepsilon + \sin^2 \varepsilon$$

ε angle between load and grain direction

$$k_{90} = \begin{cases} 1.10 & \text{in the member of the head side} \\ 1.20 & \text{in the member of the point side} \end{cases}$$

ρ_k characteristic density of the wooden member in kg/m^3

d outer thread diameter of the screw in mm

The Equations above may be applied for ESSVE screws within single softwood layers in cross laminated timber, if the single layer is considered as a separate softwood member and the minimum spacing, end and edge distances are observed for the single layer. Hereby, ρ_k is the characteristic density of the cover layer.

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The characteristic embedment strength of ESSVE screws in the narrow face of cross laminated timber may be determined independent of the angle between screw axis and grain direction as

$$f_{h,k} = 20 \cdot d^{-0.5}$$

unless otherwise specified in the technical specification of the cross laminated timber.

A.6.2.4 Slip modulus for screws loaded perpendicular to the screw axis

The slip modulus $K_{ser,v}$ per shear joint for the serviceability limit state shall be taken for screws independent of angle α to the grain as

$$K_{ser,v} = k_v \cdot d^{1.7} \text{ in N/mm}$$

with

k_v coefficient depending on the direction of load on the type of the connection and the predrilling according to Table A6.14

Table A6.14: Coefficient k_v depending on the direction of load on the type of the connection and the predrilling

Direction of load	Non-predrilled		Pre-drilled	
	Wood-wood	Metal-wood	Wood-wood	Metal-wood
Parallel to the direction of the grain $K_{ser,v,0}$	32	64	$1.6 \cdot \rho_k^{0.5}$	$3.2 \cdot \rho_k^{0.5}$
Perpendicular to the direction of the grain $K_{ser,v,90}$	16	32	$0.8 \cdot \rho_k^{0.5}$	$1.6 \cdot \rho_k^{0.5}$

Linear interpolation is possible for arbitrary angles between load direction and angle of the grain.

For the connection of two wooden members with different characteristic densities ρ_k for the determination of k_v may be determined by

$$\rho_k = \sqrt{\rho_{k,1} \cdot \rho_{k,2}}$$

with

$\rho_{k,1}$ characteristic density of wooden member 1 in kg/m^3

$\rho_{k,2}$ characteristic density of wooden member 2 in kg/m^3

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A.7 ESSVE screws in selected steel-wood and wood-wood connections

A.7.1 Steel-wood connections

Design for equally tightened screws (torque controlled) in a steel member under an angle $30^\circ \leq \alpha \leq 60^\circ$ (see Figure A7.1) may follow:

$$F_{\alpha,Rd} = F_{ax,Rd} \cdot (\cos \alpha + \mu \cdot \sin \alpha)$$

with

$$F_{ax,Rd} = n_{ef} \cdot \min \left\{ \begin{array}{l} f_{ax,calc,k} \cdot d \cdot l_{ef} \cdot \frac{k_{mod}}{\gamma_M} \\ \frac{f_{tens,k}}{\gamma_{M2}} \end{array} \right.$$

where:

- $F_{\alpha,Rd}$ load bearing capacity of inclined screws in N
- n_{ef} effective number of screws according to A.6.1.1
- k_{mod} modification factor for duration of load and moisture content according to EN 1995-1-1
- γ_M partial safety factor for connections according to EN 1995-1-1
- γ_{M2} partial safety factor according to EN 1993-1-1
- α angle between screw axis and grain direction
- μ friction coefficient between steel member and timber surface, $\mu = 0.3$

NOTES:

- 1) The real thread length of the screw is to be considered.
- 2) Occurring tensile stresses perpendicular to grain have to be verified for $h_{ef} : h < 0.7$. A related reinforcement with fully threaded ESSVE screws is shown in Figure A7.1.
- 3) For arrangement of the ESSVE screws perpendicular to the grain verification shall follow Clause A.6.2.
- 4) For combined loading (more than one loading component to be transferred by the screwed joint) the regulations according to A6.3 shall be considered.

Figure A7.1 shows an example of metal-to-timber connection with inclined ESSVE Screws located in the end-grain or in side-grain.

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Bending beams under flexible jointing	

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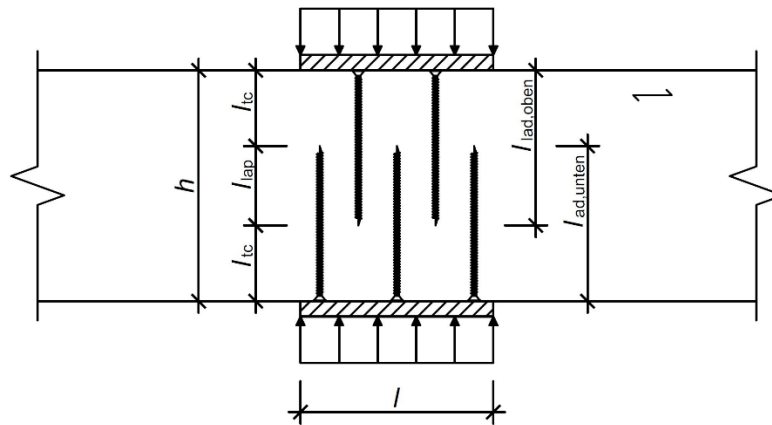


Figure A8.2: Reinforcement of timber members loaded in compression perpendicular to the grain for load transfer

A.8.2 Reinforcement of timber members loaded in tension perpendicular to the grain

Fully threaded screws may be used as tensile reinforcement perpendicular to the grain of the timber members. The screws are driven into the timber member under an angle between the screw axis and the grain direction of 90°. A minimum of two screws shall be used for tensile reinforcement perpendicular to the grain. Only one screw may be used when the minimum penetration depth of the screws below and above the potential crack is 20 · d where d is the outer thread diameter of the screw.

A.8.2.1 Tension reinforcement for transverse connections and notches

Tension reinforcement of transverse connections and notches in wooden members may be designed as follows:

$$1.3 \cdot V_d \cdot \left[3 \cdot \left(1 - \frac{h_{ef}}{h} \right)^2 - 2 \cdot \left(1 - \frac{h_{ef}}{h} \right)^3 \right] \leq F_{ax,Rd} \quad \text{for notches}$$

$$F_{90,Ed} \cdot \left[1 - 3 \cdot \left(\frac{a}{h} \right)^2 + 2 \cdot \left(\frac{a}{h} \right)^3 \right] \leq F_{ax,Rd} \quad \text{for transverse connections}$$

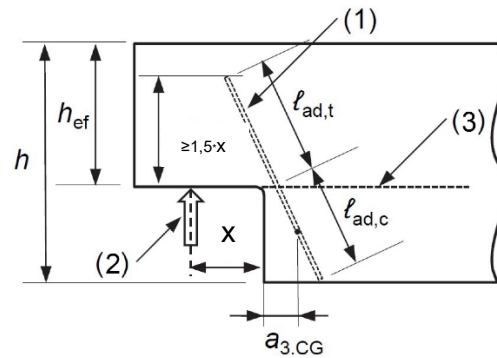
where

$$F_{ax,Rd} = n_{90} \cdot \min \left\{ \begin{array}{l} f_{ax,k} \cdot d \cdot l_{ef} \cdot \frac{k_{mod}}{\gamma_M} \\ \frac{f_{tens,k}}{\gamma_{M2}} \end{array} \right. \quad \text{for reinforcement acc. to Figure A8.3 and A8.4}$$

- V_d design value of the lateral force in N
- $F_{90,Ed}$ design value of the force acting in the connection perpendicular to the grain of the timber members in N
- h_{ef} effective height/thickness of the timber member above the notch in mm
- h height/thickness of the timber member in mm
- a distance of the furthest fastener of the transverse connection from the loaded edge of the wooden member in mm (Figure A8.4)

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- (1) inclined fully threaded screw
- (2) application of load at the support
- (3) plane of the potential crack

Figure A8.3: Reinforcement of notches with screws arranged under an angle of 90° or inclined screws

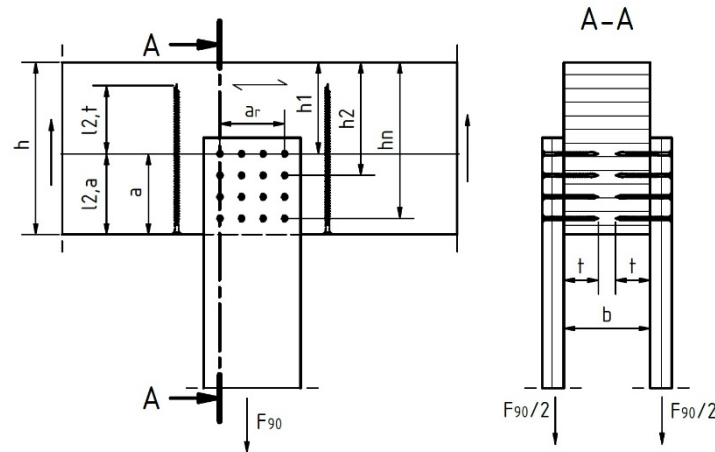


Figure A8.4: Reinforcement of transverse connections with ESSVE screws

A.8.2.2 Openings

Openings in wooden members may be designed as follows:

$$F_{t,V,d} + F_{t,M,d} \leq F_{ax,Rd}$$

where

$$F_{t,V,d} = \frac{V_d \cdot h_d}{4 \cdot h} \cdot \left(3 - \frac{h_d^2}{h^2} \right)$$

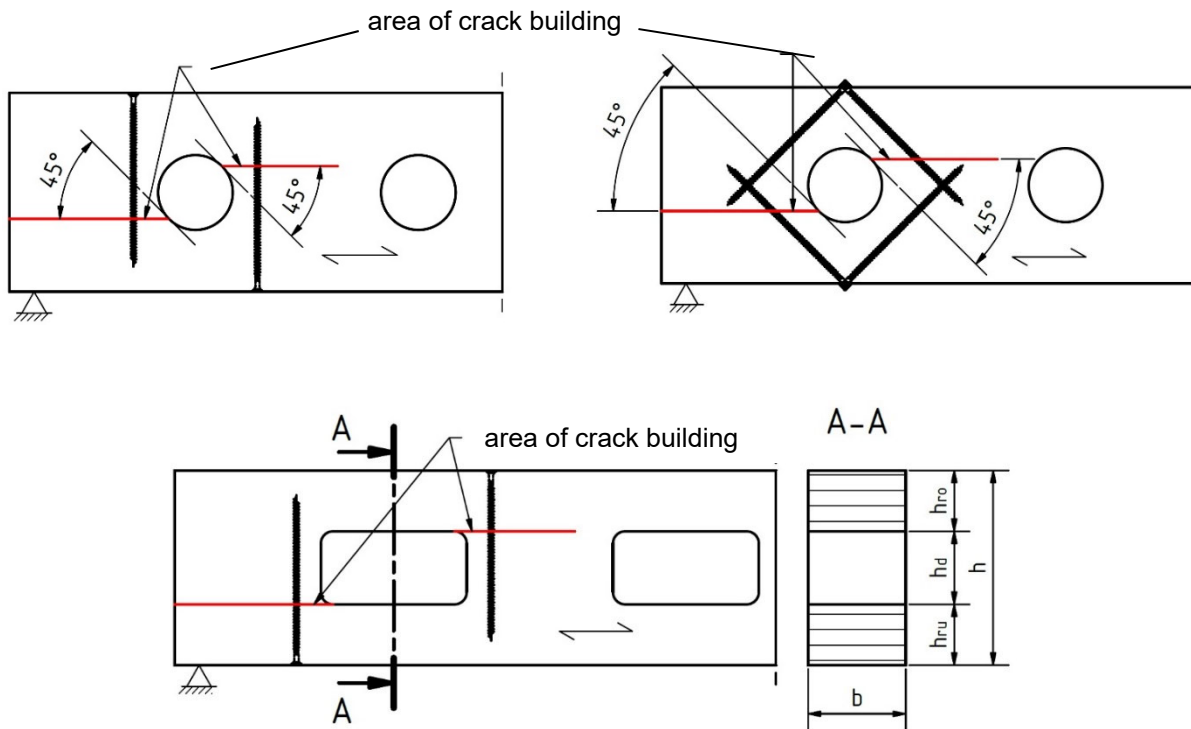
$$F_{t,M,d} = 0.008 \cdot \frac{M_d}{h_r}$$

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$$F_{ax,Rd} = n_{90} \cdot \min \left\{ \begin{array}{l} f_{ax,k} \cdot d \cdot l_{ef} \cdot \frac{k_{mod}}{\gamma_M} \\ \frac{f_{tens,k}}{\gamma_{M2}} \end{array} \right. \text{ for reinforcement acc. to Figure A8.5}$$

with

- $F_{t,V,d}$ design value of tension force perpendicular to the grain due to lateral force V_d in N
- $F_{t,M,d}$ design value of tension force perpendicular to the grain due to bending moment M_d in N
- h_d height of the opening for rectangular openings or 70 % of opening diameter for circular openings in mm
- h_r min (h_{ro} ; h_{ru}) for rectangular openings or min ($h_{ro} + 0.15 h_d$; $h_{ru} + 0.15 h_d$) for circular openings in mm
- l_{ef} smaller value of the penetration depth below or above the plane of the potential crack in mm
- k_{mod} modification factor for duration of load and moisture content according to EN 1995 1-1
- γ_M partial safety factor for connections according to EN 1995-1-1, Table 2.3
- γ_{M2} partial safety factor according to EN 1993-1-1
- n_{90} number of reinforcing screws arranged in a row perpendicular to the grain



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A.8.2.4 Shear reinforcement

Fully threaded screws may be used as shear reinforcement of solid timber, glued laminated timber and glued solid timber of softwood. The provisions are valid for straight beams with constant rectangular cross-section. The screws are driven into the timber member under an angle between the screw axis and the grain direction of 45°.

A minimum of four screws shall be used for shear reinforcement in a line parallel to the grain whereas the spacing between the screws shall not exceed the depth *h* of the timber member. If the screws are arranged in one line parallel to the grain, it shall be done centrally in relation to the beam width.

The effect of the reinforcement is limited to the shaded part of the timber member. Outside this area sufficient shear strength of the cross section must be verified.

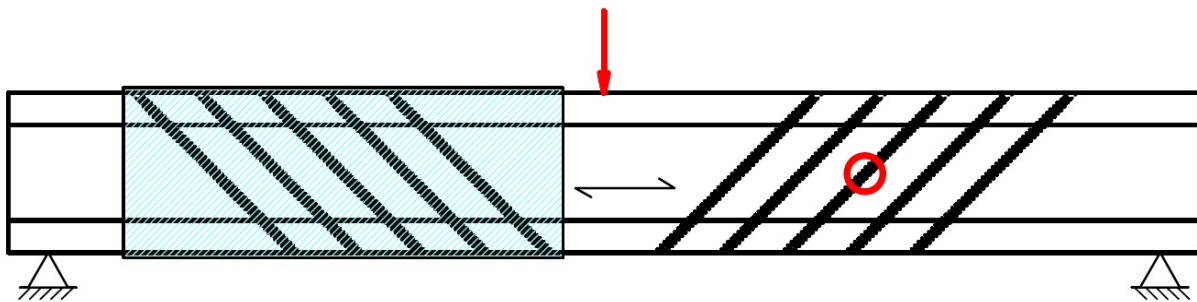


Figure A8.7: Shear reinforcement with ESSVE screws

Shear reinforcement may be designed according to

$$\tau_d \leq \frac{f_{v,d} \cdot \kappa_\tau}{\eta_H}$$

where

τ_d design value of shear stress in N/mm²

$f_{v,d}$ design value of shear strength in N/mm²

$$\kappa_\tau = 1 - 0.46 \cdot \sigma_{90,d} - 0.052 \cdot \sigma_{90,d}^2$$

$\sigma_{90,d}$ design value of stress perpendicular to the grain in N/mm²

$$\sigma_{90,d} = \frac{F_{ax,d}}{\sqrt{2} \cdot b \cdot a_1}$$

b width of the timber member in mm

*a*₁ spacing of screws parallel to the grain in mm

$$F_{ax,d} = \frac{\sqrt{2} \cdot (1 - \eta_H) \cdot V_d \cdot a_1}{h}$$

*V*_d design shear force in N

h height of the timber member in mm

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A.9.1 Fastening of thermal insulation material (on top of rafters and facades)

ESSVE screws with an outer thread diameter of at least 6 mm and lengths between 120 mm and 600 mm may be used for fixing of thermal insulation material on rafters or on wood-based members in vertical facades. Screws with partial thread and cylinder head are excluded from fixing wood-based panels on rafters with thermal insulation material as interlayer.

The angle between grain direction and screw axis shall be $30^\circ \leq \alpha \leq 90^\circ$.

The thickness of the **thermal insulation material** is max. 400 mm. The thermal insulation material shall be applicable as insulation on top of rafters according to national provisions that apply at the installation site.

The **battens** are made from solid timber strength class C24 according to EN 338 and EN 14081-1. The minimum thickness and width of the battens is:

Table A9.1 Minimum thickness and width of the battens

Screw diameter d in mm	b_{min}	t_{min}
	mm	mm
≤ 8	50	30
10	60	40
12	80	50

Instead of battens the following **wood-based panels** may be used to cover the thermal insulation material if they are suitable for that use:

- Plywood according to EN 636 and EN 13986,
- Oriented Strand Board, OSB according to EN 300 and EN 13986,
- Particleboard according to EN 312 and EN 13986
- Fibreboards according to EN 622-2, EN 622-3 and EN 13986.

The minimum thickness of the wood-based panels shall be 22 mm.

The word batten in the following includes the meaning of the above mentioned wood-based panels.

The **substructure** is made from solid timber strength class C24 according to EN 338 and EN 14081-1, cross laminated timber according to European Technical Assessments or laminated veneer lumber according to EN 14374. The minimum width is $b_{min} = 60$ mm, for screws with an outer thread diameter of 12 mm the minimum width $b_{min} = 80$ mm.

The spacing between screws e_s shall be not more than 1.75 m.

Friction forces shall not be considered for the design of the characteristic axial capacity of the screws.

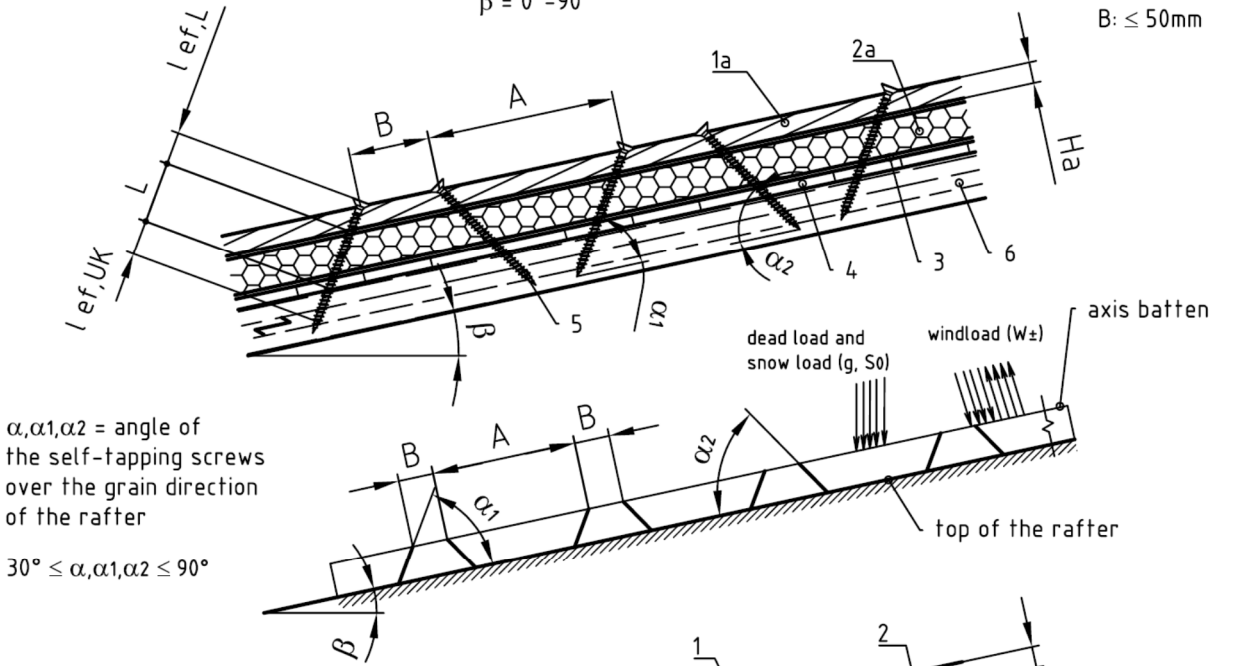
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Version 1

roof, facade
 $\beta = 0^\circ - 90^\circ$

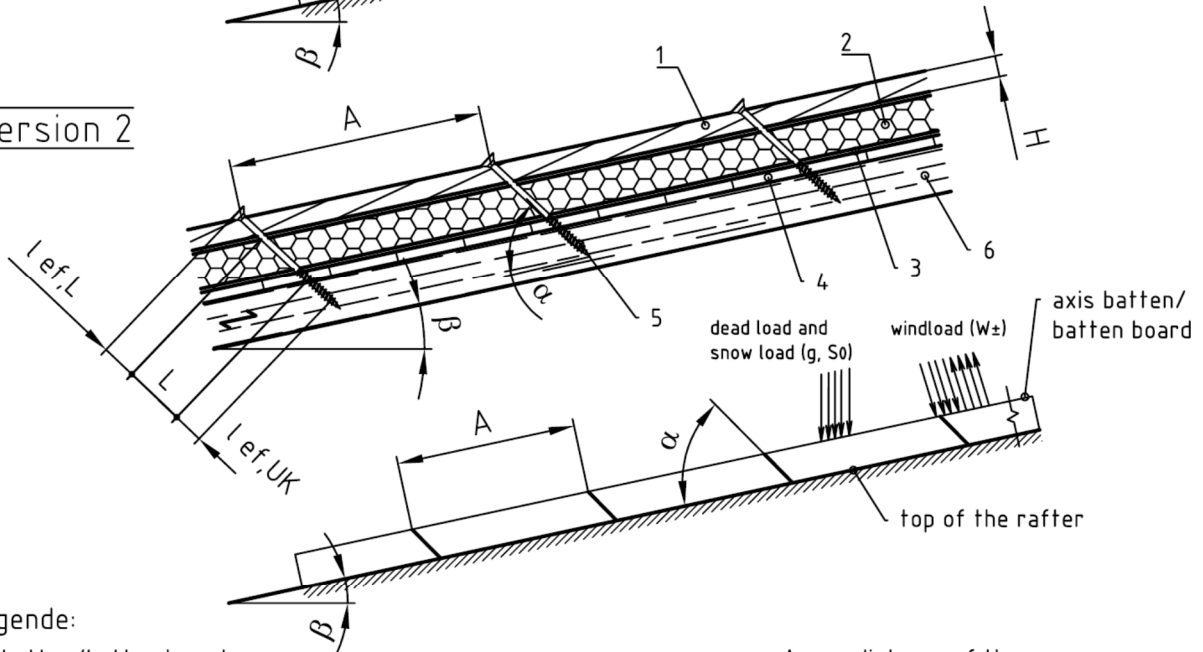
A: acc. to statics
B: $\leq 50\text{mm}$



$\alpha, \alpha_1, \alpha_2 =$ angle of the self-tapping screws over the grain direction of the rafter

$30^\circ \leq \alpha, \alpha_1, \alpha_2 \leq 90^\circ$

Version 2



Legende:

- 1 batten/batten board
- 1a batten
- 2 heat insulation (till 300mm), pressure resistant (min. 0,05 N/mm²)
- 2a heat insulation (till 400mm), pressure resistant
- 3 vapour barrier
- 4 roof boards
- 5 self-tapping screws
- 6 rafter

- A distance of the screws
- H thickness batten/batten board
- Ha thickness batten
- l ef,L penetration length in the batten/batten board
- l ef,UK penetration length in the rafter

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Table A9.2 Buckling capacity of the screws

Free screw length <i>l</i> between lath and rafter (mm)	$\kappa_c * N_{pl,k}$ (kN) for ESSVE screws			
	Outer thread diameter <i>d</i>			
	6	8	10	12
	Inner thread diameter <i>d_i</i>			
	3.8	5.2	6.2	6.9
≤35	4.396	11.681	19.024	25.125
60	2.497	7.576	13.516	18.834
80	1.706	5.416	10.070	14.470
100	1.232	4.008	7.621	11.154
120	0.930	3.068	5.912	8.747
140	0.726	2.418	4.699	7.000
160	0.582	1.952	3.815	5.710
180	0.477	1.608	3.156	4.739
200	0.398	1.347	2.652	3.992
220	0.337	1.144	2.259	3.407
240	0.289	0.984	1.947	2.941
260	0.251	0.855	1.695	2.563
280	0.220	0.750	1.489	2.254
300	0.194	0.663	1.318	1.997
320	-	0.591	1.175	1.781
340	-	0.529	1.054	1.599
360	-	0.477	0.950	1.443
380	-	0.432	0.862	1.309
400	-	0.393	0.785	1.193

A.9.3 Parallel inclined screws

The screws are predominantly loaded in tension whereas corresponding thermal insulation material is loaded in compression. The minimum compression stress of the thermal insulation material at 10 % deformation, measured according to EN 826, shall be $\sigma_{(10\%)} \geq 0.05 \text{ N/mm}^2$. Hereby systems with battens or wood-based panels may be used.

Design

For design of thermal insulation systems in terms of number and spacing of the screws the following characteristic withdrawal parameter may be taken into account:

$$R_{ax,k} = \min \left\{ \begin{array}{l} f_{ax,k,\alpha} \cdot d \cdot l_{ef,UK} \cdot k_1 \cdot k_2 \\ \max \left\{ \begin{array}{l} f_{head,k} \cdot d_k^2 \\ f_{ax,k,\alpha} \cdot l_{ef,L} \cdot d \end{array} \right. \end{array} \right. \quad \text{in N}$$

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European Assessment Document EAD 130118-01-0603 “Screws and threaded rods for use in timber constructions”

EN 300 (07.2006), Oriented Strand Boards (OSB) – Definitions, classification and specifications

EN 312 (09.2010), Particleboards – Specifications

EN 338 (04.2016), Structural timber – Strength classes

EN 622-2 (04.2004) +AC (12.2005), Fibreboards – Specifications – Part 2: Requirements for hardboards

EN 622-3 (04.2004), Fibreboards – Specifications – Part 3: Requirements for medium boards

EN 634-1 (03.1995), Cement-bonded particleboards – Specifications – Part 1: General requirements

EN 636:2012+A1 (03.2015), Plywood – Specifications

EN 826 (03.2013), Thermal insulating products for building applications – Determination of compression behaviour

EN 1993-1-4 (10.2006) +A1 (06.2015), Eurocode 3 – Design of steel structures – Part 1-4: General rules – Supplementary rules for stainless steels

EN 1995-1-1 (11.2004), +AC (6.2006), +A1 (06.2008), +A2 (05.2014), Eurocode 5 – Design of timber structures – Part 1-1: General – Common rules and rules for buildings

EN 10088-1 (10.2014), Stainless steels – Part 1: List of stainless steels

EN 13353:2008+A1 (05.2011), Solid wood panels (SWP) – Requirements

EN 13986:2004+A1 (04.2015), Wood-based panels for use in construction - Characteristics, evaluation of conformity and marking

EN 14080 (06.2013), Timber structures – Glued laminated timber and glued solid timber – Requirements

EN 14081-1:2016+A1 (08.2019), Timber structures – Strength graded structural timber with rectangular cross section – Part 1: General requirements

EN 14374 (11.2004), Timber structures – Structural laminated veneer lumber – Requirements

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Reference documents	